

1 SYMBOLS AND ABBREVIATIONS

1.1 Symbols

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1.3 Abbreviations

1 SYMBOLS AND ABBREVIATIONS

1.1	<u>Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
A	Parameter defined in Section 13.1.5	°C	°F
$A_b$	Fluidised bed cross sectional area	$m^2$	$ft^2$
$A_e$	Constant in elutriation equation 9.3	-	-
$A_t$	Total surface area of in-bed tubing for heat transfer: based on tube OD.	$m^2$	$ft^2$
$A_s$	Sorbent additive Reactivity Index	-	-
Ar	Archimedes number	-	-
$Ar_{mf}$	Archimedes number at minimum fluidising conditions	-	-
$Ar_t$	Archimedes number at terminal velocity	-	-
$A_w$	Flow area of packed bed	$m^2$	$ft^2$
a	Bed area supplied per coal feed point	$m^2$	$ft^2$
$a_o$	Constant	$m^{-2}$	(ft h)/(gal s)
B	Volume fraction of bed occupied by tube bank	-	-
$B_h$	Fraction of bed height occupied by tube bank	-	-
$B_l$	Parameter defined in Section 13.1.5	-	-
b	Index in feed solids size distribution equation	-	-
$b_o$	Constant	m/s	ft/s
$C'$	Weight fraction of carbon in fuel	-	-
Ca	Weight fraction of calcium in sorbent	-	-
C	Fractional combustion (fraction of potential heat input)	-	-
$C_b$	combustion occurring in bed		
$C_d$	datum loss from bed surface		
$C_f$	combustion in freeboard		

<u>Symbols</u>	<u>Units</u>	
	<u>SI</u>	<u>British</u>
$C_J$	loss from the bed surface corrected for the coal mixing parameter	
$C_o$	total loss from bed surface	
$C_{oc}$	loss of feed coal from bed surface	
$C'_o$	total loss from surface of fines burn-up bed	
$C_{of}$	loss of recycled carbon fines from bed surface	
$C'_c$	loss from bed surface assuming coal feed only	
$C_t$	loss in combustor off-gas	
$C_r$	ratio of recycled carbon fines to carbon in coal feed	
$C_D$	Drag coefficient	-
$C_{N_{ox}}$	$NO_x$ concentration	ppm v/v
$C_{O_2}$	Oxygen concentration in the flue gas	% v/v
$c_b$	Specific heat of bed material	J/(kg °K)      Btu/(lb°F)
$C_d$	Orifice pressure drop constant	-
$c_g$	Mean specific heat of gas and entrained solids (defined in Section 13.1.5)	J/(kg °K)      Btu/(lb°F)
$c_i$	Percentage of coal in the i th. size fraction	-
$D$	Oil nozzle body inside diameter	mm              in.
$D_b$	Bubble diameter	m                m
$D_d$	Diameter of exit holes in air nozzles	mm              ft
$D_E$	Oil nozzle exit hole diameter	mm              in.
$D_i$	In-bed heat transfer tubing, inside diameter	mm              inches
$D_o$	In-bed heat transfer tubing, outside diameter	mm              inches
$D_t$	Thermal diffusivity	m <sup>2</sup> /s            ft <sup>2</sup> /h

	<u>Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
D <sub>A</sub>	Axial oil tube outside diameter	mm	in.
D <sub>M</sub>	Hydraulic diameter of nozzle body flow path	mm	in.
d	Particle size (diameter)	µm	inches
	d <sub>Mx</sub> maximum particle size defined so that 99% w/w of the sample is smaller than d <sub>Mx</sub>		
	d <sub>A</sub> maximum particle size used in sorbent characterisation test		
	d <sub>c</sub> effective particle size below which elutriation is assumed to be instantaneous		
	d <sub>i</sub> ) particle size of i th. and j th. fractions d <sub>j</sub> )		
	d <sub>m</sub> particle size where f = 1 for the straight line approximation to the coarse particle size distribution		
	$\bar{d}_p$ surface mean particle size of bed		
	d <sub>r</sub> size below which particles pass through the recycle fines collector		
	d <sub>t</sub> particle of size having its terminal velocity equal to the operating fluidising velocity		
	d <sub>x</sub> mean particle size of x th. fraction	m	ft
E	Activation energy	J/kg mol	Btu/lb mol
E <sub>H</sub>	Gross calorific value of fuel	kJ/kg	Btu/lb
E <sub>x</sub>	Elutriation rate constant	kg/(sm <sup>2</sup> )	lb/(hft <sup>2</sup> )

<u>Symbols</u>	<u>Units</u>	
	<u>SI</u>	<u>British</u>
$e_a$	Constant in feed solids size distribution equation	$\mu\text{m}^{-1}$ inches <sup>-1</sup>
$e$	Sulphur oxides emission )	In appropriate units
$e_o$	Statutory permissible sulphur oxides emission )	See Section 11.3.1.4
$F$	Total feed rate of inert bed material	kg/(sm <sup>2</sup> )                  lb/(h ft <sup>2</sup> )
$F_n$	Fluidisability number = $Ar^{1/3}$	-                          -
$F_s$	Bed temperature as a fraction of the bed to tube temperature difference	-                          -
$\bar{F}_s$	Mean bed value of $F_s$	-                          -
$F_T$	Factor for deviations from counter current flow	-                          -
$f$	Fraction of undersize material: Fanning friction factor	-                          -
$f_a$	Fraction by weight of abraded fines below size $d_c$	-                          -
$f_b$	Weight fraction of input calcium remaining in the bed	-                          -
$f_c$	Fraction by weight of fine material below size $d_c$	-                          -
$f_e$	Weight fraction of input calcium elutriated	-                          -
$f_r$	Fraction of material below size $d_r$ , lost through recycle collector	-                          -
$f_R$	Fractional change to new steady state sulphur retention	-                          -
$f_x$	Volume fraction of voids less than particle size $d_x$ also- equals $f_b^x$ or $f_e$ as appropriate See Section 11.3.4.2	-                          -

	<u>Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
G	Mass flow per unit area per unit time	kg/(s m <sup>2</sup> )	lb/(h ft <sup>2</sup> )
	G <sub>A</sub> additive flow		
	G <sub>F</sub> flow of feed solids below size d <sub>c</sub>		
	G <sub>a</sub> air flow		
	G <sub>ac</sub> flow of elutriated particles produced by the abrasion of larger particles to size d <sub>c</sub>		
	G <sub>c</sub> fuel flow		
	G <sub>e</sub> total elutriation rate from bed		
	G <sub>g</sub> total gas flow		
	G <sub>h</sub> ash flow		
	G <sub>r</sub> flow of make-up solids		
	G <sub>x</sub> flow of fines elutriated for fraction of size d <sub>x</sub>		
	G <sub>l</sub> flow of fines produced by abrasion in recycle stream		
g	Gravitation constant	m/s <sup>2</sup>	ft/s <sup>2</sup>
H'	Weight fraction of hydrogen in fuel	-	-
H <sub>r</sub>	Net heat of reaction of sulphur retention additive	kW	Btu/h
H <sub>r1</sub>	Heat of sulphation of CaCO <sub>3</sub>	kW	Btu/h
H <sub>r2</sub>	Heat of calcination of the MgCO <sub>3</sub> content of the sorbent	kW	Btu/h
H <sub>r3</sub>	Heat of calcination of the CaCO <sub>3</sub> content of the sorbent	kW	Btu/h
H <sub>L</sub>	Overall heat loss due to sulphur retention sorbent	kW	Btu/h
H <sub>s</sub>	Net sensible heat loss due to sulphur retention sorbent	kW	Btu/h
H <sub>se</sub> , H <sub>sb</sub>	Sensible heat loss in the spent sorbent in the elutriated solids and overflow bed material streams respectively	kJ/kg	Btu/lb

<u>Symbols</u>	<u>Units</u>	
	<u>SI</u>	<u>British</u>
$H_6$	Sensible heat loss in the $CO_2$ evolved by the sorbent	$kJ/kg$ $Btu/lb$
$H_7$	Sensible heat loss in the $SO_2$ and $O_2$ taken up by the sorbent	$kJ/kg$ $Btu/lb$
$h$	Hydrostatic head, ie depth of bed + height of water level above bed surface	$m$ $ft$
$h_c$	Outside film heat transfer coefficient convection component	$J/(s\ m^2\ ^\circ K)$ $Btu/(ft^2h\ ^\circ F)$
$h_i$	Inside film heat transfer coefficient	$J/(s\ m^2\ ^\circ K)$ $Btu/(ft^2h\ ^\circ F)$
$h_o$	Total outside film heat transfer coefficient	$J/(s\ m^2\ ^\circ K)$ $Btu/(ft^2h\ ^\circ F)$
$h_r$	Outside film heat transfer coefficient, radiation component	$J/(s\ m^2\ ^\circ K)$ $Btu/(ft^2h\ ^\circ F)$
$I_1$ ) $I_2$ )	Constants in equation 9.25	-      -
$J^2$	Coal mixing parameter	(atm m)
$K$	Combustion reaction velocity constant	$s^{-1}$ $s^{-1}$
$K_A$	Abrasion constant	$s\ m/s$ $h\ ft/s$
$K_{am}$	Weight mean value of $K_A$	$s\ m/s$ $h\ ft/s$
$K_{ar}$	Recycle abrasion constant	-      -
$K_p$	Equilibrium constant for reaction 11.65	$(kN/m^2)^{-1/2}$ $(atm)^{-1/2}$
$K_s$	Ratio of the tube spacing to tube outside diameter	-      -
$K_w$	Coefficient of water permeability in packed beds	$m/day$ $ft/s$
$k$	Thermal conductivity	$J/(m\ s\ ^\circ K)$ $Btu/(ft\ h\ ^\circ F)$
$k_e$	Calcium elutriation constant	See equation 11.33
$k_r$	Constant in equation 11.33	See equation 11.33
$k_s$	Constant in equation 11.8	-      -
$k_o$	Datum value of $k_s$	-      -
$k_x$	Constant in size reduction rate equation	$(\mu m\ s)^{-1}$ $(in\ h)^{-1}$

<u>Symbols</u>	<u>Units</u>	
	<u>SI</u>	<u>British</u>
$k_1$ to $k_5$	Reaction velocity constants. See Section 12.	
	$\text{cm}^3/(\text{g mol s})$	
L	Height of cooled freeboard wall:	m ft
	Height of heat transfer surface:	m ft
	Slumped height of bed solids in tapered portion of the bed	m ft
$L_b$	Expanded bed height	m ft
$L_{mf}$	Expanded bed height at minimum fluidising conditions	m ft
$L_n$	Length of oil nozzle	mm in.
$L_s$	Packed bed height: Slumped bed height	m ft
$L_1, L_2$	Expanded bed heights at two levels in a fluidised bed	m ft
l	Total immersed length of in-bed tubing	m ft
$l_o$	Vertical path of circulating particles in the bed	m ft
M	Mass flow rate per unit time	kg/s lb/h
$M_a$	input air flow	
$M_x$	fuel flow	
$M_{cs}$	stoichiometric fuel flow	
$M_g$	air plus fuel flow	
$M_s$	sorbent flow	
$M_{sb}$	flow of spent sorbent retained by the bed	
$M_{se}$	flow of spent sorbent elutriated	
$M_{lx}$ to $M_{5x}$	mass flows of calcium sulphate ( $M_1$ ), magnesium oxide ( $M_2$ ), calcium oxide ( $M_3$ ), calcium carbonate ( $M_4$ ), and inert impurities ( $M_5$ ) in the elutriated sorbent ( $x = e$ ), or the sorbent remaining in the bed ( $x = b$ ).	



<u>Symbols</u>	<u>Units</u>		
	<u>SI</u>	<u>British</u>	
$M_6$	mass flow of $\text{CO}_2$ evolved from the sorbent		
$M_7$	mass flow of $\text{SO}_2 + \text{O}_2$ absorbed by the sorbent		
Mg	Weight fraction of magnesium in the sorbent	-	
$m_e$	Mol fraction of sulphur oxides in wet flue gas	-	
$m_d, m_w$	Mol fractions of sulphur oxides in the dry and wet combustor off gas respectively assuming that all the sulphur in the fuel enters the gas	-	
$m_{ij}$	Fraction by weight of ash prepared from coal in size fraction j which is in size fraction i	-	
$m_{\text{H}_2\text{O}}$	Mol fraction of water	-	
$m_{\text{SO}_2}$	Mol fraction of sulphur dioxide	-	
$m_{\text{SO}_3}$	Mol fraction of sulphur trioxide	-	
N	Number of coal feed points:	-	
	Number of oil exit holes per nozzle	-	
Nu	Nusselt number	-	
n	Maximum number of oil nozzle exit holes per row	-	
O	Solids overflow rate	kg/(s m <sup>2</sup> )	lb/(h ft <sup>2</sup> )
O'	Weight fraction of oxygen in fuel	-	-
O <sub>x</sub>	Fuel oxygen content, wt %		% dmmf
P	Operating pressure (absolute)	kN/m <sup>2</sup>	atm
P <sub>c</sub>	Actual carbon dioxide partial pressure	kN/m <sup>2</sup>	atm

	<u>Symbols</u>	<u>Units</u>	
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$P_{ce}$	Equilibrium carbon dioxide partial pressure	kN/m <sup>2</sup>	atm
$P_{O_2}$	Partial pressure of oxygen leaving the bed	kN/m <sup>2</sup>	atm
$P_{SO_2}$	Partial pressure of sulphur dioxide leaving the bed	kN/m <sup>2</sup>	atm
$Pr$	Prandtl number	-	-
$P_i$	Percentage of the total ash occurring in the <i>i</i> th. size fraction	-	-
$P$	Parameter = $(b-1)/b$	-	-
$P_h$	In-bed tubing horizontal tube pitch	mm	inches
$P_v$	In-bed tubing vertical tube pitch	mm	inches
$Q$	Heat flow per unit time	J/s	Btu/h
	$Q_c$ due to combustion in bed and freeboard		
	$Q_g$ removed from the bed by the off-gas and elutriated ash at temperature $T_b$		
	$Q_r$ rate of heat transfer by radiation		
	$Q_t$ rate of heat transfer by in-bed tubing		
	$Q_1-Q_6$ terms in the freeboard heat balance. See Section 4.3.2.2		
$q$	Parameter = $(b\beta - 1)/b$	-	-
$q_i$	Relative proportion of ash in the <i>i</i> th. fraction		
$R$	Gas constant	cal/(°K g mol)	
$R$	Ratio, $\frac{\text{cross-sectional area of tube}}{\text{total area of holes}}$	-	-
$R$	Fractional reduction by weight of SO <sub>2</sub>	-	-
	$R_a$ by additive		
	$R_c$ by coal ash		
$R_e$	Reynolds number	-	-

	<u>Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
Re <sub>mf</sub>	Reynolds number at minimum fluidising conditions	-	-
Re <sub>t</sub>	Reynolds number at terminal velocity conditions	-	-
r	Radius in Section 10.5. Also Decrepitation parameter	mm	inches
r <sub>c</sub>	Effective calcium carbonate calcination rate		
r <sub>m</sub>	Effective magnesium carbonate calcination rate		
r <sub>o</sub>	Effective calcium carbonate calcination rate at zero carbon dioxide partial pressure		See Section 11.3.3.2
r <sub>r</sub>	Sorbent recycle parameter		
S'	Weight fraction of sulphur in fuel		
T	Temperature	°C	°F
T <sub>a</sub>	freeboard temperature		
T <sub>ai</sub>	temperature of slice i of the freeboard		
T <sub>b</sub>	bed temperature		
T <sub>bo</sub>	bed temperature at time zero		
T <sub>boo</sub>	bed temperature at new steady state		
T <sub>bt</sub>	bed temperature at time t		
T <sub>e</sub>	freeboard exit temperature		
T <sub>f</sub>	bulk cooling fluid temperature		
T <sub>i</sub>	in-bed tubing inner surface temperature		
T <sub>p</sub>	air preheat temperature		
T <sub>w</sub>	in-bed tubing outer surface temperature		
$\bar{T}$	mean bed value of T		

	<u>Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
T'	Absolute temperature	°K	°R
	T' <sub>a</sub> freeboard temperature		
	T' <sub>b</sub> bed temperature		
	T' <sub>d</sub> sulphuric acid dew point		
	T' <sub>w</sub> tube wall temperature		
	T' <sub>A</sub> sorbent characterisation test temperature		
	T' <sub>IN</sub> Turbine inlet temperature		
t	Time	s	h
t <sub>c</sub>	Time constant	s	h
t <sub>f</sub>	Mean freeboard gas residence time	s	s
t <sub>g</sub>	Superficial gas residence time in the bed: In Section 5 on slumped bed basis	s	s
t <sub>m</sub>	Mean residence time needed for the sorbent to achieve a sulphation fraction, $\kappa_a$	s	s
t <sub>s</sub>	Time taken to reach new steady state conditions	s	s
t <sub>A</sub>	Duration of sorbent characterisation test	h	h
U	Overall heat transfer coefficient	J/(m <sup>2</sup> s °K)	Btu/(ft <sup>2</sup> h °F)
U <sub>b</sub>	Bubble rise velocity	m/s	ft/s
U <sub>d</sub>	Velocity through exit holes of air distributor nozzles	m/s	ft/s
U <sub>f</sub>	Fluidising velocity	m/s	ft/s
U <sub>mf</sub>	Minimum fluidising velocity	m/s	ft/s
U' <sub>f</sub>	Gas velocity in tube bank	m/s	ft/s
U <sub>sl</sub>	Superficial spray exit velocity	m/s	ft/s
U' <sub>sl</sub>	Spray limited exit velocity	m/s	ft/s
U <sub>t</sub>	Terminal velocity	m/s	ft/s

<u>Symbols</u>	<u>Units</u>		
	<u>SI</u>	<u>British</u>	
V	Oil flow per oil nozzle:	m <sup>3</sup> /s	Imp gal/h
	Water volumetric flowrate through packed beds	m <sup>3</sup> /d	ft <sup>3</sup> /s
V <sub>a</sub>	Inlet air volume at mean bed conditions	m <sup>3</sup> /s	ft <sup>3</sup> /s
V <sub>ao</sub>	Air flow per oil nozzle	m <sup>3</sup> /s	ft <sup>3</sup> /s
V <sub>B</sub>	Bubble volume fraction	-	-
V <sub>f</sub>	Freeboard volume	m <sup>3</sup>	ft <sup>3</sup>
V <sub>n</sub>	Velocity number = $Re/Ar^{1/3}$	-	-
V <sub>o</sub>	Oil flow per oil nozzle exit hole	m <sup>3</sup> /s	Imp gal/h
V <sub>t</sub>	Tube volume fraction	-	-
V <sub>w</sub>	Molar volume		
	specific values are:	m <sup>3</sup> /kg mol	ft <sup>3</sup> /lb mol
	22.7 m <sup>3</sup> per kg mole at 0°C and 100 kN/m <sup>2</sup>		
	22.4 l per g mole at 0°C and 1 atm		
	359 ft <sup>3</sup> per lb mole at 32°F and 1 atm		
	379 ft <sup>3</sup> per lb mole at 60°F and 1 atm		
v	Linear air velocity in nozzle body	m/s	ft/s
W	Total bed weight	kg	lb
W <sub>b</sub>	Bed weight per unit area	kg/m <sup>2</sup>	lb/ft <sup>2</sup>
W <sub>Ca</sub>	Weight of calcium in the bed at steady-state conditions	kg	lb
W <sub>x</sub>	Weight of particles of size d <sub>x</sub> in bed per unit area	kg/m <sup>2</sup>	lb/ft <sup>2</sup>
w	Bed width at base of taper	m	ft
w <sub>a</sub>	Stoichiometric moles of air required for combustion of unit weight of fuel	kg mol/kg	lb mol/lb
w <sub>d</sub>	Moles of dry gas given by the combustion of unit weight of fuel	kg mol/kg	lb mol/lb

	<u>Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
$w_w$	Moles of wet gas given by the combustion of unit weight of fuel	kg mol/kg	lb mol/lb
X	Excess air; % of stoichiometric amount ie $X = \frac{\text{actual air} - \text{stoichiometric air}}{\text{stoichiometric air}} \times 100$	%	%
x	Tube thickness in equation 10.3a:	m	ft
	tube length in equation 10.17	m	ft
$X_e$	Effective excess air; % of stoichiometric amount	%	%
$X_s$	Excess gas velocity in the dense phase	m/s	ft/s
$X_i$ ) $x_j$ )	Weight fraction of i th. and j th. fractions	-	-
$x_{ij}$	Weight of fraction between sizes $d_i$ and $d_j$	-	-
y	Variable in error function definition	-	-
Y	Additive Ca/S molar ratio	-	-
Z	Mol ratio $\text{MgCO}_3/\text{CaCO}_3$ in sulphur retention sorbent	-	-
$Z_b$	Bed depth correction factor	-	-
$Z_n$	Nozzle density per unit bed area	$\text{m}^{-2}$	$\text{ft}^{-2}$
$Z_t$	Bed taper effectiveness factor	-	-
z	Spacing between heat transfer tubing	mm	inches
$z_h$	Distance above distributor plate	mm	inches

1.2	<u>Greek Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
$\alpha$	Additive constant	-	-
$\beta$	Parameter defined by equation 9.20	-	-
$\gamma$	Fraction by weight of carbon fines leaving the bed that is collected	-	-
$\delta$	Fraction of heat present at a given height in the freeboard which is returned to the bed	-	-
$\delta_s$	Ratio of the observed to the equilibrium value of $K_p$	-	-
$\Delta P_1$	Pressure differential between two points at depths $L_1$ and $L_2$ in a fluidised bed	kN/m <sup>2</sup>	atm
$\Delta P_2$	Pressure differential between a point at depth $L_2$ in a fluidised bed and a point in the freeboard	kN/m <sup>2</sup>	atm
$\Delta P_b$	Pressure drop through the bed	kN/m <sup>2</sup>	atm (or in. H <sub>2</sub> O)
$\Delta P_d$	Pressure drop through the distributor	kN/m <sup>2</sup>	atm (or in. H <sub>2</sub> O)
$\Delta P_f$	Pressure drop through the freeboard	kN/m <sup>2</sup>	atm (or in. H <sub>2</sub> O)
$\Delta T$	Logarithmic mean temperature difference	°C	°F
$\epsilon_b$	Bed emissivity	-	-
$\epsilon_h$	Emissivity	-	-
$\epsilon_{mf}$	Voidage at minimum fluidising conditions	-	-
$\zeta$	Fuel type parameter	-	-
$\eta$	Overall combustion efficiency	%	%
$\theta$ ) $\theta_1$ ) $\theta_2$ ) $\theta$	Units change constants Also, Angle in cylindrical coordinate system; See Section 10.5		As appropriate
$\kappa$	Fraction of sorbent sulphated	-	-
$\kappa_A$	Fraction of sorbent sulphated in sorbent characterisation test	-	-

1.2	<u>Greek Symbols</u>	<u>Units</u>	
		<u>SI</u>	<u>British</u>
$\kappa_a$	Average fraction of sorbent sulphated	-	-
$\kappa_b$	Fractional sulphation of the calcium remaining in the bed	-	-
$\kappa_e$	Fractional sulphation of the elutriated calcium	-	-
A	Bubble size index	-	-
$\lambda$	Fraction of carbon leaving the bed caught by the recycle cyclone	-	-
$\mu$	Gas viscosity	Ns/m <sup>2</sup>	lb/(fts)
$\zeta$	Fuel type parameter	-	-
$\pi$	Ratio, circumference/diameter of circle	-	-
$\rho$	Fixed bed bulk density	kg/m <sup>3</sup>	lb/ft <sup>3</sup>
$\rho_f$	Fluidised bed mean bulk density	kg/m <sup>3</sup>	lb/ft <sup>3</sup>
$\rho_{mf}$	Fluidised bed density at minimum fluidising conditions	kg/m <sup>3</sup>	lb/ft <sup>3</sup>
$\rho_g$	Gas density	kg/m <sup>3</sup>	lb/ft <sup>3</sup>
$\rho_s$	Particle density	kg/m <sup>3</sup>	lb/ft <sup>3</sup>
$\sigma$	Stefan Botzmann radiation constant	J/(m <sup>2</sup> s °K <sup>4</sup> )	Btu/(ft <sup>2</sup> h °F <sup>4</sup> )
$\phi$	Sphericity of particle	-	-
$\chi$	Sulphation rate constant	-	-
$\chi'$	Sulphation rate constant	-	-
$\psi$	Variable in error function definition	-	-
$\Omega$	Power in equation 4.4	-	-



1.3 Abbreviations

BCURA British Coal Utilisation Research Association  
(now CURL)

BP British Petroleum Company Limited,  
including Research Laboratories, Sunbury

CRE National Coal Board, Coal Research Establishment

CSL Combustion Systems Limited

CURL National Coal Board, Coal Utilisation Research  
Laboratories

NCB National Coal Board

  

FBC Fluidised Bed Combustion

MCR Maximum Continuous Rating

METR Maximum Effective Thickness Reduction